# Cubic-Plus-Association Equation of State for Water-Containing Mixtures: Is "Cross Association" Necessary?

Zhidong Li and Abbas Firoozabadi

Reservoir Engineering Research Institute (RERI), Palo Alto, CA 94306

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We have recently proposed an accurate version of the cubic-plus-association (CPA) equation of state (EOS) for water-containing mixtures which combines the Peng-Robinson equation (PR) for the physical interactions and the thermodynamic perturbation theory for the hydrogen bonding of water molecules. Despite the significant improvement, the water composition in the nonaqueous phase is systematically underestimated for some systems where the nonwater species are methane and ethane at very high pressures, unsaturated hydrocarbons,  $CO_2$ , and  $H_2S$ . We attribute the deficiency to the neglect of the "cross association" between water and those nonwater molecules. In this work, the accuracy is drastically improved by treating methane, ethane, unsaturated hydrocarbons,  $CO_2$  and  $H_2S$  as "pseudo-associating" components and describing the cross association with water in the framework of the perturbation theory. It is shown that the cross association is more significant for the nonaqueous phase. In addition to binary mixtures, reliable predictions are achieved for  $H_2O/C_1/CO_2/H_2S$  quaternary mixture in two and three phases. © 2009 American Institute of Chemical Engineers AIChE J, 55: 1803–1813, 2009

Keywords: petroleum, phase equilibrium, aqueous solutions

#### Introduction

The importance of water-containing mixtures is widely recognized in many disciplines particularly in the fields of energy and environment. However, it has been challenging to accurately describe the phase behavior of such systems by using theoretical approaches due to complicated nonidealities from the strong hydrogen bonding of water molecules. The cubic-plus-association (CPA) equation of state (EOS) is a powerful tool compared with alternatives<sup>1</sup>; the existing versions demonstrate only limited success due to the poor per-

formance for some cases [Li ZD and Firoozabadi A (2008); Sun LX and Firoozabadi A (2006)].<sup>2–6</sup>

In a recent work, we have proposed an accurate version of CPA for water-containing mixtures in which the physical contribution and the hydrogen bonding of water molecules are described by the Peng-Robinson equation (PR) and the thermodynamic perturbation theory (TPT), respectively. By introducing the higher order temperature-dependent corrections to estimate the energy parameter of pure water in the physical part, the accuracy is drastically improved. The improvement is demonstrated by comparing the calculations and experiments for various binary, ternary and quaternary water/saturated-hydrocarbon mixtures in two and three phases under a wide range of temperatures and pressures.<sup>7</sup>

Despite the significant improvement, the composition of water in the nonaqueous phase is systematically underestimated for nonwater species including methane and ethane at very high pressures, unsaturated hydrocarbons, CO<sub>2</sub>, and

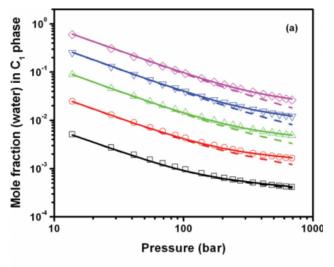
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A. Firoozabadi is also affiliated with Dept. of Chemical Engineering, Yale University, New Haven, CT 06520.

Correspondence concerning this article should be addressed to A. Firoozabadi at

abbas.firoozabadi@yale.edu

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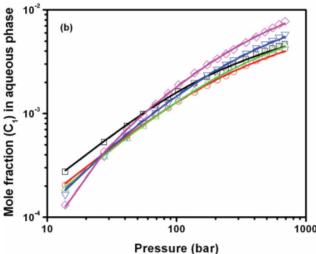


Figure 1. Compositions of (a)  $C_1$  phase and (b) aqueous phase of  $H_2 O/C_1$  mixture.

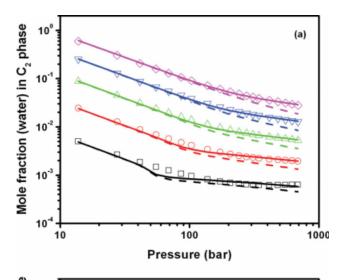
 $C_1$  phase is vapor. Symbols represent experiments from Refs. 19, 20. Solid and dashed lines represent calculations with and without cross association, respectively. Symbols  $\square$ ,  $\bigcirc$ ,  $\triangle$ ,  $\bigtriangledown$  and  $\diamondsuit$  along with corresponding lines are for 310.93, 344.26, 377.59, 410.93, and 444.26 K, respectively. [Color figure can be viewed in the online issue, which is available at www.interscience.wiley.com.]

H<sub>2</sub>S. The deviation from the experiments becomes very large especially for mixtures containing aromatic hydrocarbons, CO<sub>2</sub> and H<sub>2</sub>S in the liquid–liquid phase region. We ascribe this deficiency to the neglect of an explicit cross association with water beyond the physical interactions. The origin of the cross association can be either from the water-induced temporary polar moments of hydrocarbon molecules or from the permanent polar moments of CO<sub>2</sub> and H<sub>2</sub>S molecules. For the nonwater species examined, we suspect that H<sub>2</sub>S has the strongest cross association energy with water, followed by aromatic hydrocarbons and CO<sub>2</sub>, and then alkenes. For saturated hydrocarbon components, the cross association with water could be negligible except for methane and ethane at very high pressures.<sup>7</sup>

In this work, we improve our original CPA approach by applying the "pseudo-association" concept to explicitly consider the cross association between water and nonwater species. R-12 The remainder of this article is organized as the following. We first introduce the molecular modeling and the basic formalism of the theory for the pseudo-association. Next, the performance is illustrated by comparison with the experiments for the phase compositions of H<sub>2</sub>O/C<sub>1</sub>, H<sub>2</sub>O/C<sub>2</sub>, H<sub>2</sub>O/CO<sub>2</sub>, H<sub>2</sub>O/H<sub>2</sub>S, H<sub>2</sub>O/1-hexene, H<sub>2</sub>O/1-octene, H<sub>2</sub>O/1-decene, H<sub>2</sub>O/benzene, H<sub>2</sub>O/2-dethylbenzene, H<sub>2</sub>O/m-diethylbenzene, H<sub>2</sub>O/1-methylnaphthalene, and H<sub>2</sub>O/C<sub>1</sub>/CO<sub>2</sub>/H<sub>2</sub>S mixtures in two and three phases. Based on accurate description of the phase behavior, the density change when water is saturated with CO<sub>2</sub> is also investigated. The work is concluded with some remarks.

# Molecular Modeling and Theoretical Background

We consider the mixtures with nonwater species such as linear 1-alkenes, aromatic hydrocarbons, methane, ethane,



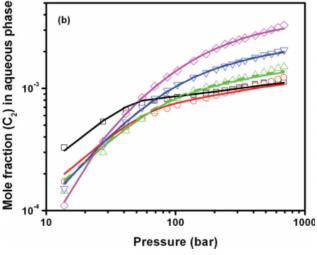
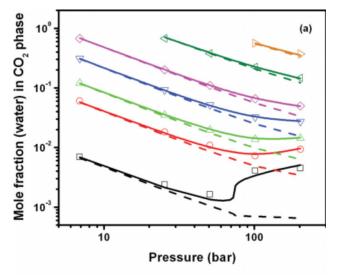


Figure 2. Same as Figure 1 but for H<sub>2</sub>O/C<sub>2</sub> mixture.

 $\mathrm{C}_2$  phase can be either vapor or liquid. Experiments are from Refs. 21, 22. [Color figure can be viewed in the online issue, which is available at www.interscience.wiley.com.]



represent the mole fractions of water and pseudo-associating component i, respectively.  $\chi_{\alpha}(\chi_{\beta})$  is the mole fraction of water not bonded at site " $\alpha$ " (" $\beta$ ") and  $\chi_{\alpha_i}'(\chi_{\beta_i}')$  is the mole fraction of pseudo-associating component i not bonded at site " $\alpha_i$ " (" $\beta_i$ ").

We also make two other assumptions. First, there is neither cross association nor self association between pseudo-associating components, i.e., the "association strength"  $\Delta^{\alpha_i \beta_j} = 0$ . Second, the cross association is assumed to be symmetric between two sites of different types of water and pseudo-associating component i, i.e.,  $\Delta^{\alpha \beta_i} = \Delta^{\alpha_i \beta}$ . For the symmetric four-site association model for both the water and the pseudo-associating molecules, the nonbonded mole fractions can be calculated from the simplified expressions of the perturbation theory

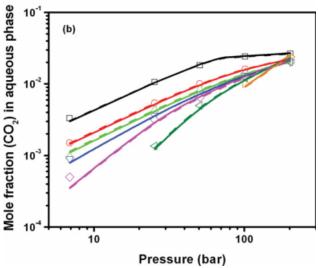


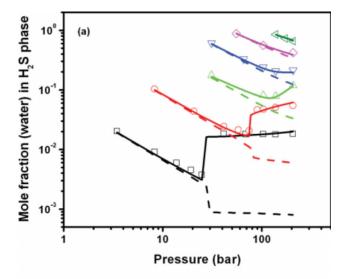
Figure 3. Same as Figure 1 but for  $H_2O/CO_2$  mixture.

 $CO_2$  phase can be either vapor or liquid. Experiments are from Ref. 23. Symbols  $\square$ ,  $\bigcirc$ ,  $\triangle$ ,  $\bigtriangledown$ ,  $\diamondsuit$ ,  $\vartriangleleft$  and  $\triangleright$  along with corresponding lines are for 304.21, 348.15, 366.48, 394.26, 422.04, 477.59 and 533.15 K, respectively. [Color figure can be viewed in the online issue, which is available at www.interscience.wiley.com.]

 ${\rm CO_2}$ , or  ${\rm H_2S}$  or any combination and treat these substances as pseudo-associating components. Similar to water molecules, each pseudo-associating molecule is assumed to possess four association sites belonging to two types ( $\alpha_i'$  and  $\beta_i'$ ) with two sites for each type. As a result, the excess Helmholtz free energy due to association is given by  $^{13-18}$ 

$$\frac{F_{\text{ass}}^{\text{ex}}}{nRT} = 2x_{\text{w}} \left( \ln \chi_{\alpha} + \ln \chi_{\beta} - \frac{\chi_{\alpha} + \chi_{\beta}}{2} + 1 \right) + \sum_{i} 2x_{\text{ci}} \left( \ln \chi_{\alpha'_{i}} + \ln \chi_{\beta'_{i}} - \frac{\chi_{\alpha'_{i}} + \chi_{\beta'_{i}}}{2} + 1 \right) \tag{1}$$

where n is the total number of moles, R is the universal gas constant, and T is the absolute temperature.  $x_{\rm w}$  and  $x_{\rm ci}$ 



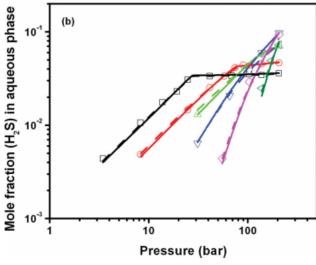
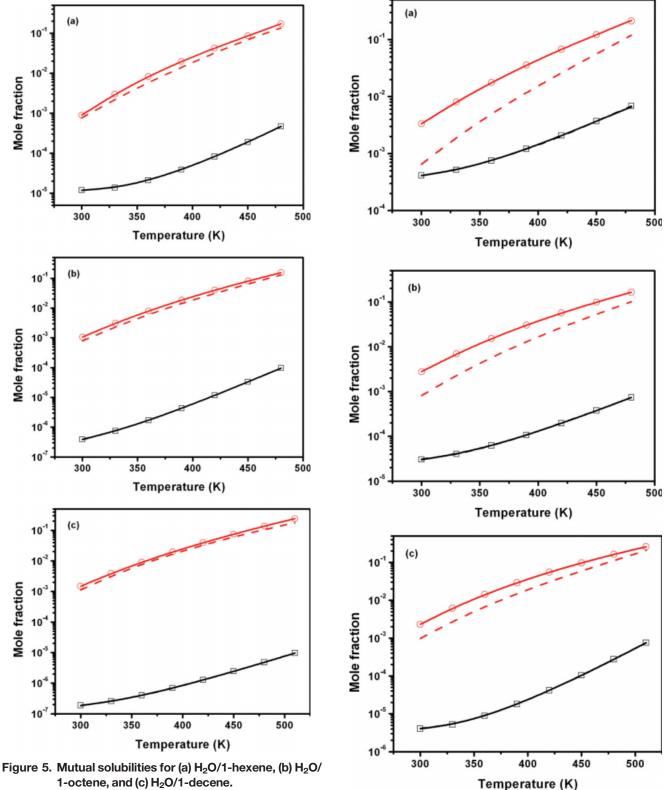


Figure 4. Same as Figure 1 but for  $H_2O/H_2S$  mixture.

 $H_2S$  phase can be either vapor or liquid. Experiments are from Ref. 23. Symbols  $\square,\bigcirc,\triangle,\bigtriangledown,\diamondsuit$  and  $\vartriangleleft$  along with corresponding lines are for 310.93, 366.48, 422.04, 477.59, 533.15 and 588.71K, respectively. [Color figure can be viewed in the online issue, which is available at www.interscience.wiley.com.]

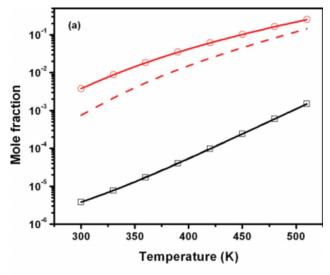


1-octene, and (c) H<sub>2</sub>O/1-decene.

Symbols represent experiments or calibrations from Ref. 24. Solid and dashed lines represent calculations with and without cross association, respectively. Symbols  $\square$  and  $\bigcirc$  along with corresponding lines are the solubilities of hydrocarbon in water and of water in hydrocarbon, respectively. [Color figure can be viewed in the online issue, which is available at www.interscience.wiley.com.]

Figure 6. Same as Figure 5 but for (a) H<sub>2</sub>O/Benzene, (b) H<sub>2</sub>O/Ethylbenzene, and (c) H<sub>2</sub>O/m-diethylben-

Experiments or calibrations are from Refs. 24–26. [Color figure can be viewed in the online issue, which is available at www.interscience.wiley.com.]



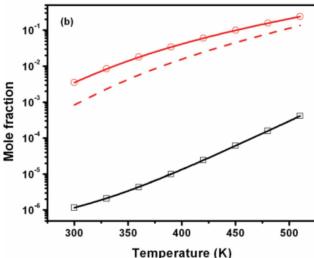


Figure 7. Same as Figure 5 but for (a) H<sub>2</sub>O/1-methylnaphthalene, and (b) H<sub>2</sub>O/1-ethylnaphthalene.

Experiments or calibrations are from Ref. 24. [Color figure can be viewed in the online issue, which is available at www.interscience.wiley.com.]

$$\chi_{\alpha} = \chi_{\beta} = \chi = \frac{1}{1 + 2\rho x_{\rm w} \chi \Delta^{\alpha\beta} + \sum_{i} 2\rho x_{\rm ci} \chi_{i}' \Delta^{\alpha\beta_{i}'}}$$
(2a)

$$\chi_{\alpha_i'} = \chi_{\beta_i'} = \chi_i' = \frac{1}{1 + 2\rho x_{\mathbf{w}} \chi \Delta^{\alpha \beta_i'}}$$
 (2b)

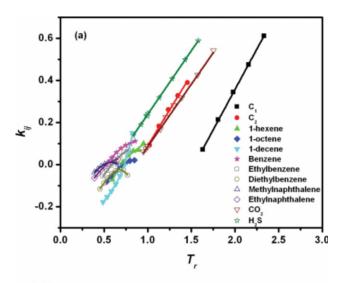
where  $\rho$  is the molar density. As a consequence, Eq. 1 is further simplified to

$$\frac{F_{\text{ass}}^{\text{ex}}}{nRT} = 4x_{\text{w}} \left( \ln \chi - \frac{\chi}{2} + \frac{1}{2} \right) + \sum_{i} 4x_{\text{ci}} \left( \ln \chi_{i}' - \frac{\chi_{i}'}{2} + \frac{1}{2} \right). \quad (3)$$

Between molecules of water, the association strength is given by  $\Delta^{\alpha\beta}=g\kappa^{\alpha\beta}$  [exp  $(\varepsilon^{\alpha\beta}/k_{\rm B}T)-1$ ]. Here,  $k_{\rm B}$  is the Boltzmann constant, and  $\kappa^{\alpha\beta}$  and  $\varepsilon^{\alpha\beta}$  are the bonding volume and energy parameters of water, respectively. g is the contact

value of the radial distribution function of hard-sphere mixture which can be approximated by that of the pure hardsphere fluid as  $g \approx \frac{1-0.5\eta}{(1-\eta)^3}$  with  $\eta = \frac{b\rho}{4}$  and b the molecular volume parameter. Between molecules of water and pseudoassociating component i, the association strength is simply related to that between water molecules, i.e.,  $\Delta^{\alpha\beta'_i} = s_i \Delta^{\alpha\beta}$ where the temperature-dependent cross association factor  $s_i$ can be determined by fitting the experiments of binary mixtures together with the binary interaction coefficients  $k_{\rm ii}$ .  $^{10,11}$ 

The methodology proposed above results in a unified model which drastically simplifies the computations. Other cross association schemes also can be used in modeling the pseudo-associating components. Two-site model is mathematically equivalent to the four-site model. However, onesite and three-site models will invalidate Eq. 2 and therefore complicate the computations. In the absence of water, the



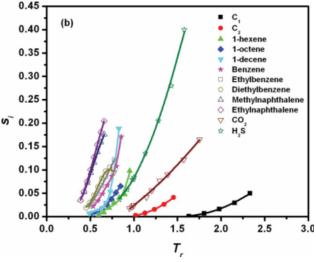


Figure 8. (a) Binary interaction coefficients and (b) cross association factors between water and non-water components as a function reduced temperature of non-water species.

Lines are for guidance. [Color figure can be viewed in the online issue, which is available at www.interscience.wiley.

Table 1. Mole Fractions of Water in C<sub>1</sub> Phase for H<sub>2</sub>O/C<sub>1</sub> Mixture at High Pressures

	Mole Fraction of Water in C <sub>1</sub> Phase								
		758.4 bar		896.3 bar					
	Exp	Cal(ca)	Cal(nca)	Exp	Cal(ca)	Cal(nca)			
313.9 K	4.72e-4	4.79e-4	4.22e-4	4.67e-4	4.57e-4	3.99e-4			
366.5 K	3.13e-3	3.37e-3	2.29e-3	2.88e-3	3.21e-3	2.09e-3			
422.04 K	0.0143	0.0159	0.0100	0.0137	0.0151	8.89e-3			
466.5 K	0.040	0.0425	0.0273	_	_	_			
477.5 K	0.051	0.0528	0.0344	_	-	_			
		965.3 bar			1103.2 bar				
466.5 K	0.035	0.0391	0.0227	0.033	0.0376	0.0206			
477.5 K	0.0494	0.0486	0.0285	0.0455	0.0466	0.0258			

Experiments are from Ref. 27.

The columns with labels "ca" and "nca" represent the predictions with and without cross association, respectively.

resulting expression reduces to that of the original PR-EOS which has been successfully applied to the compositional reservoir simulators in the phase behavior calculations for hydrocarbon mixtures.

#### **Results and Discussion**

In Figures 1–4, we calculate the phase compositions for  $H_2O/C_1$ ,  $^{19,20}$   $H_2O/C_2$ ,  $^{21,22}$   $H_2O/CO_2$ ,  $^{23}$  and  $H_2O/H_2S^{23}$  binary mixtures. For H<sub>2</sub>O/C<sub>1</sub> mixture, the equilibrium is between the vapor and aqueous phases. For H<sub>2</sub>O/C<sub>2</sub>, H<sub>2</sub>O/CO<sub>2</sub>, and H<sub>2</sub>O/H<sub>2</sub>S mixtures, the jumps for the water composition in the nonaqueous phase at low temperatures are due to the change of the nonaqueous phase from vapor to liquid. It should be noted that for H<sub>2</sub>O/C<sub>2</sub> mixture the sharp transition of the nonaqueous phase is hard to distinguish from the experiments. There is a slight decrease for H<sub>2</sub>O/C<sub>2</sub> mixture but a substantial increase for H<sub>2</sub>O/CO<sub>2</sub> and H<sub>2</sub>O/H<sub>2</sub>S mixtures of the water composition in the nonaqueous phase. The sudden transition corresponds to the appearance of the vapor-liquid-liquid three-phase point which disappears at high temperatures. To facilitate the comparison, the results without cross association are also presented.<sup>7</sup> The experiments are always perfectly reproduced and the accuracy is independent of the cross association in the aqueous phase.

The accuracy of water mole fraction in the nonaqueous phase is greatly improved when cross association is taken into account. The calculated results with cross association are in excellent agreement with the experiments especially for H<sub>2</sub>O/CO<sub>2</sub> and H<sub>2</sub>O/H<sub>2</sub>S mixtures in the liquid-liquid phase region. For H<sub>2</sub>O/C<sub>1</sub> and H<sub>2</sub>O/C<sub>2</sub> mixtures, the cross association is negligible when the pressure is not very high (e.g., lower than 200 bar), and, thus, the computations can be simplified.

Figures 5-7 present calculations and experiments for the mutual solubilities of H<sub>2</sub>O/1-hexene, H<sub>2</sub>O/1-octene, H<sub>2</sub>O/1decene, H<sub>2</sub>O/benzene, H<sub>2</sub>O/ethylbenzene, H<sub>2</sub>O/m-diethylbenzene, H<sub>2</sub>O/1-methylnaphthalene, and H<sub>2</sub>O/1-ethylnaphthalene mixtures in liquid-liquid phase region. 24-26 For comparison, the results without cross association are also exhibited. Similar to Figures 1-4, the hydrocarbon solubility in the aqueous phase is always perfectly reproduced. In the presence of cross association, the water solubility in the nonaqueous phase is drastically improved especially for the aromatic hydrocarbons.

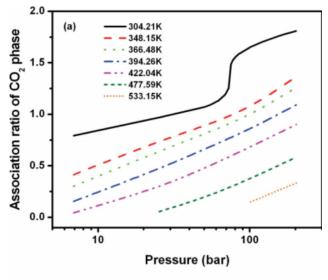
The binary interaction coefficients and cross association factors are displayed in Figure 8 as a function of the reduced temperature of the nonwater species. For water/unsaturatedhydrocarbon mixtures,  $k_{ij}$  and  $s_i$  may not be very reliable because there is only one datapoint to determine them for

Table 2. Same as Table 1 But for Mole Fractions of Water in C<sub>2</sub> Phase for H<sub>2</sub>O/C<sub>2</sub> Mixture at High Pressures

	Mole Fraction of Water in C <sub>2</sub> Phase								
		758.4 bar		896.3 bar					
	Exp	Cal(ca)	Cal(nca)	Exp	Cal(ca)	Cal(nca)			
314.8 K	4.93e-4	6.42e-4	5.00e-4	4.49e-4	6.15e-4	4.73e-4			
366.5 K	3.02e-3	3.89e-3	2.48e-3	2.87e-3	3.70e-3	2.29e-3			
422.0 K	0.01498	0.0167	0.0105	0.01382	0.0157	9.50e-3			
466.5 K	0.0455	0.0425	0.0286	_	-	_			
		965.3 bar			1103.2 bar				
466.5 K	0.0401	0.0384	0.0243	0.0372	0.0364	0.0223			

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Experiments are from Ref. 27.



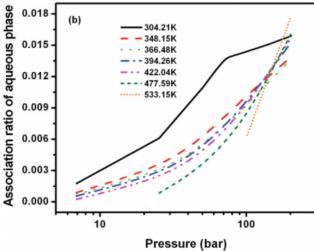
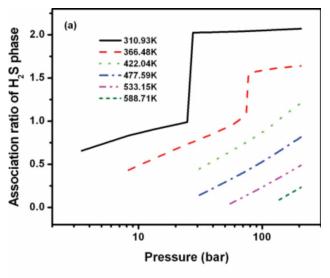


Figure 9. Association ratios of (a)  $CO_2$  phase and (b) aqueous phase of  $H_2O/CO_2$  mixture.

[Color figure can be viewed in the online issue, which is available at www.interscience.wiley.com.]

each temperature. As shown in Figure 8a, the binary interaction coefficients increase linearly with temperature for H<sub>2</sub>O/ C<sub>1</sub>, H<sub>2</sub>O/C<sub>2</sub>, H<sub>2</sub>O/CO<sub>2</sub>, and H<sub>2</sub>O/H<sub>2</sub>S mixtures. It should be noted that in our recent work, due to the neglect of the cross association, the binary interaction coefficients only slightly change for H<sub>2</sub>O/CO<sub>2</sub> mixture but decrease for H<sub>2</sub>O/H<sub>2</sub>S mixture with the increase of the temperature. Different with those of the mixtures containing only nonwater species, the binary interaction coefficients of water-containing mixtures is strongly temperature-dependent. The "apparent" dispersion attraction between water and pseudo-associating species is influenced by the degree of self- and cross-association which is very sensitive to temperature. As presented in Figure 8b, the cross association factors demonstrate the systematic increasing trend with temperature when the nonwater species is C<sub>1</sub>, C<sub>2</sub>, CO<sub>2</sub>, and H<sub>2</sub>S; the exponential term of the association strength between water molecules drops more rapidly than that between water and pseudo-associating molecules when the temperature becomes higher. For other mixtures,  $k_{ij}$  and  $s_i$  also generally increases with temperature but the trend is not as systematic as that for  $H_2O/C_1$ ,  $H_2O/C_2$ ,  $H_2O/CO_2$ , and  $H_2O/H_2S$  mixtures. Our hypothesis is verified by examining these plots, i.e., the cross association related to aromatic hydrocarbons,  $CO_2$  and particularly  $H_2S$  plays a dominant role in the determination of phase behavior. The cross association between water and saturated hydrocarbons is very weak and negligible except for  $H_2O/C_1$  and  $H_2O/C_2$  mixtures at very high pressures.

For  $H_2O/C_1$  and  $H_2O/C_2$  mixtures, the cross association with water plays a significant role at high pressures. By using the binary interaction coefficients and cross association factors as given by Figure 8, we predict the mole fraction of water in the nonaqueous phase at very high pressures for these two mixtures in the two-phase region and compare them with the experiments from Ref. 27. The data from Ref. 27 were not used to determine the binary interaction coefficients and the cross association factors. Tables 1 and 2 present the predictions with and without the cross association at



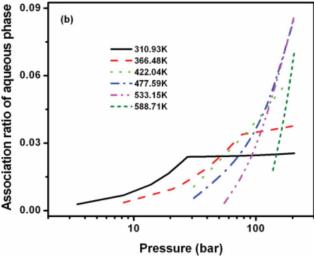


Figure 10. Same as Figure 9 but for H<sub>2</sub>O/H<sub>2</sub>S mixture.

[Color figure can be viewed in the online issue, which is available at www.interscience.wiley.com.]

Table 3. Vapor-Liquid Equilibrium of H<sub>2</sub>O/C<sub>1</sub>/CO<sub>2</sub>/H<sub>2</sub>S Mixture

			Composition (Mole Fraction)						
			<u>,                                      </u>	Aqueous			Vapor		
Temperature (K)	Pressure (bar)	Component	Exp	Cal(ca)	Cal(nca)	Exp	Cal(ca)	Cal(nca)	
310.95	48.2	$CH_4$	2.76e-4	3.23e-4	3.18e-4	0.3040	0.3024	0.3025	
		$CO_2$	9.3e-3	9.09e-3	9.43e-3	0.5945	0.5995	0.5994	
		$H_2S$	5.03e-3	4.34e-3	4.07e-3	0.0998	0.0962	0.0966	
		$H_2O$	0.9854	0.9863	0.9862	1.91e-3	1.85e-3	1.61e-3	
	76.0	$CH_4$	4.66e-4	5.16e-4	5.06e-4	0.3031	0.3040	0.3041	
		$CO_2$	0.0121	0.0124	0.0127	0.5970	0.5991	0.5989	
		$H_2S$	5.40e-3	5.40e-3	5.03e-3	0.0982	0.0954	0.0959	
		$H_2O$	0.9816	0.9817	0.9817	1.71e-3	1.48e-3	1.14e-3	
	125.2	$\overline{\mathrm{CH}_{4}}$	7.96e-4	8.65e-4	8.48e-4	0.3029	0.3043	0.3045	
		$CO_2$	0.0151	0.0147	0.0151	0.5967	0.5983	0.5983	
		$H_2S$	5.95e-3	5.38e-3	5.01e-3	0.0985	0.0959	0.0964	
		$H_2O$	0.9781	0.9791	0.9791	1.87e-3	1.60e-3	8.8e-4	
	169.3	$\widetilde{\mathrm{CH}_{4}}$	9.9e-4	1.14e-3	1.11e-3	0.3021	0.3040	0.3044	
		$CO_2$	0.0154	0.0153	0.0157	0.5963	0.5977	0.5980	
		$H_2S$	6.08e-3	4.97e-3	4.63e-3	0.0996	0.0963	0.0968	
		$H_2O$	0.9777	0.9786	0.9785	1.99e-3	2.00e-3	8.19e-4	
380.35	83.6	$\mathrm{CH_4}$	3.79e-4	3.96e-4	3.89e-4	0.2907	0.2956	0.2964	
		$CO_2$	6.98e-3	7.79e-3	7.09e-3	0.5919	0.5877	0.5899	
		$H_2S$	3.42e-3	3.26e-3	3.72e-3	0.0967	0.0953	0.0951	
		$H_2O$	0.9894	0.9886	0.9888	0.0225	0.0214	0.0185	
	129.3	$CH_4$	5.78e-4	6.12e-4	5.96e-4	0.2929	0.2980	0.2990	
		$CO_2$	9.59e-3	0.0108	9.71e-3	0.5920	0.5899	0.5929	
		$H_2S$	4.47e-3	4.17e-3	4.7e-3	0.0963	0.0952	0.0950	
		$H_2O$	0.9854	0.9844	0.9850	0.0196	0.0169	0.0131	
	171.7	$CH_4$	7.79e-4	8.02e-4	7.77e-4	0.2935	0.2990	0.3003	
		$CO_2$	0.0113	0.0128	0.0115	0.5916	0.5903	0.5940	
		$H_2S$	4.73e-3	4.65e-3	5.2e-3	0.0970	0.0952	0.0950	
		$H_2O$	0.9834	0.9817	0.9825	0.0179	0.0155	0.0108	
449.85	118.0	$\mathrm{CH_4}$	7.17e-4	7.79e-4	7.65e-4	0.2641	0.2694	0.2723	
		$CO_2$	7.95e-3	8.56e-3	8.42e-3	0.5575	0.5361	0.5419	
		$H_2S$	3.74e-3	3.73e-3	3.93e-3	0.0848	0.0868	0.0875	
		$H_2O$	0.9877	0.9868	0.9868	0.0950	0.1076	0.0982	
	173.1	$CH_4$	1.1e-3	1.17e-3	1.14e-3	0.2762	0.2775	0.2813	
		$CO_2$	0.0114	0.0119	0.0117	0.5520	0.5496	0.5571	
		$H_2S$	4.78e-3	4.90e-3	5.13e-3	0.0870	0.0885	0.0894	
		$H_2O$	0.9827	0.9820	0.9821	0.0848	0.0843	0.0722	

The overall composition of each component on mole basis is 0.15 (C<sub>1</sub>), 0.3 (CO<sub>2</sub>), 0.05 (H<sub>2</sub>S), and 0.5 (H<sub>2</sub>O). Experiments are from Ref. 28

very high pressures. For H<sub>2</sub>O/C<sub>1</sub> mixture, the consideration of cross association drastically improves the performance of CPA. For H<sub>2</sub>O/C<sub>2</sub> mixture at 314.8 and 366.5 K, the predictions without cross association are superior to those with cross association. It should be pointed out that the trend of experiments at 314.8 K from Ref. 27 is different with that at 310.93 K from Ref. 22. Such inconsistency problem does not exist between the two sets of data for H<sub>2</sub>O/C<sub>1</sub> mixture from the two references.

In this work, we have observed that the good accuracy in the aqueous phase is readily achieved compared with that of the nonaqueous phase by adjusting the binary interaction coefficients. In the aqueous phase, the solubility of nonwater species is very low and the dominant process is the self association of water molecules, which has been accurately described. In the nonaqueous phase, the concentration of water is often low, and, therefore, the cross association between water and nonwater species may not be negligible. To illustrate our point, we quantify the importance of the cross association by defining the 'association ratio' as

Association ratio (component 
$$i$$
) =  $\frac{(1 - \chi_i^{'4})x_{ci}}{(1 - \gamma^4)x_w}$ . (4)

In Eq. 4, the numerator is the number of moles of component i cross associated with water, and the denominator is the number of moles of associated water. A higher value of the association ratio implies more significant cross association. Figures 9 and 10 present the association ratios in the two phases for H<sub>2</sub>O/CO<sub>2</sub> and H<sub>2</sub>O/H<sub>2</sub>S binary mixtures. The association ratio in the nonaqueous phase is always one or two orders of magnitude larger than that of the aqueous phase, which supports our assessment that cross association is the key element in the nonaqueous phase. Moreover, the cross association becomes more important with increased pressure or when the nonaqueous phase is liquid.

The columns with labels 'ca' and 'nca' represent the predictions with and without cross association, respectively.

Table 4. Same as Table 3 But the Overall Composition is 0.05 (C<sub>1</sub>), 0.05 (CO<sub>2</sub>), 0.4 (H<sub>2</sub>S), and 0.5 (H<sub>2</sub>O)

					(mole fraction)	ole fraction)			
			Aqueous			Vapor/H <sub>2</sub> S Liquid			
Temperature (K)	Pressure (bar)	Component	Exp	Cal(ca)	Cal(nca)	Exp	Cal(ca)	Cal(nca)	
310.95	130.0	CH <sub>4</sub>	8.59e-4	9.75e-4	8.88e-4	0.0891	0.1013	0.1021	
		$CO_2$	3.62e-3	2.74e-3	2.68e-3	0.0994	0.0991	0.0998	
		$H_2S$	0.0291	0.0303	0.0271	0.8016	0.7882	0.7972	
		$H_2O$	0.9666	0.9659	0.9693	9.32e-3	0.0114	8.49e-4	
	164.6	$CH_4$	8.82e-4	1.04e-3	9.46e-4	0.0891	0.1013	0.1022	
		$CO_2$	3.81e-3	2.83e-3	2.76e-3	0.1061	0.0993	0.1001	
		$H_2S$	0.0281	0.0306	0.0273	0.7958	0.7873	0.7968	
		$H_2O$	0.9672	0.9655	0.9690	9.05e-3	0.0121	8.31e-4	
380.35	75.6	$CH_4$	1.55e-4	1.60e-4	1.56e-4	0.1182	0.0980	0.0988	
		$CO_2$	1.25e-3	1.43e-3	1.27e-3	0.1112	0.0966	0.0975	
		$H_2\tilde{S}$	0.0304	0.0289	0.0315	0.7485	0.7809	0.7843	
		$H_2O$	0.9682	0.9695	0.9670	0.0253	0.0244	0.0194	
	122.7	$\overline{\mathrm{CH}_{4}}$	3.32e-4	3.44e-4	3.21e-4	0.1060	0.1008	0.1022	
		$CO_2$	2.26e-3	2.26e-3	1.96e-3	0.1148	0.0984	0.1000	
		$H_2S$	0.0361	0.0372	0.0399	0.7528	0.7778	0.7850	
		$H_2O$	0.9613	0.9600	0.9577	0.0264	0.0229	0.0127	
	169.2	$\overline{\mathrm{CH}_{4}}$	6.06e-4	5.78e-4	5.18e-4	0.1207	0.1002	0.1029	
		$CO_2$	3.34e-3	2.81e-3	2.43e-3	0.1176	0.0978	0.1006	
		$H_2S$	0.0392	0.0384	0.0417	0.7322	0.7709	0.7861	
		$H_2O$	0.9568	0.9582	0.9554	0.0295	0.0311	0.0104	
449.85	110.0	$\mathrm{CH}_4$	3.50e-4	3.36e-4	3.12e-4	0.1092	0.0905	0.0924	
		$CO_2$	1.64e-3	1.69e-3	1.56e-3	0.1078	0.0892	0.0912	
		$H_2\tilde{S}$	0.0286	0.0341	0.0334	0.6896	0.6979	0.7126	
		$H_2O$	0.9694	0.9638	0.9647	0.0938	0.1224	0.1037	
	181.7	$\widetilde{\text{CH}_4}$	7.15e-4	7.16e-4	6.12e-4	0.0928	0.0933	0.0967	
		$CO_2$	2.92e-3	2.95e-3	2.55e-3	0.0914	0.0909	0.0944	
		$H_2S$	0.0517	0.0520	0.0484	0.704	0.7112	0.7379	
		$H_2O$	0.9454	0.9433	0.9485	0.113	0.1035	0.0710	

At 310.95K, the equilibrium is between the aqueous phase and H<sub>2</sub>S liquid phase.

On the basis of binary interaction coefficients and cross association factors presented above without any adjustments, we perform the predictions for phase composition of H<sub>2</sub>O/C<sub>1</sub>/CO<sub>2</sub>/H<sub>2</sub>S quaternary mixture in two- and three-phase regions. Results are displayed in Tables 3–5.<sup>28</sup> Here, the cross association between water and C<sub>1</sub> is not accounted for because the pressure is lower than 200 bar. The binary interaction coefficients of H<sub>2</sub>O-C<sub>1</sub>, C<sub>1</sub>-CO<sub>2</sub>, C<sub>1</sub>-H<sub>2</sub>S and CO<sub>2</sub>-H<sub>2</sub>S can be found in.<sup>7,29,30</sup> For the comparison purpose, the results without cross association are also presented.<sup>7</sup> Similar to binary mixtures, the prediction of water mole fraction in the vapor phase and particularly in the H<sub>2</sub>S liquid phase is significantly improved with cross association. The accuracy is nearly unaffected for other components. The effect of

cross association to this quaternary mixture is highlighted by the average absolute deviations (AAD) shown in Table 6.

Accurate description of the density of water saturated with  $\mathrm{CO}_2$  is very important in modeling of  $\mathrm{CO}_2$  sequestration and migration in saline aquifers, oceans, and depleted oil and gas reservoirs and in the simulation of  $\mathrm{CO}_2$ -related enhanced oil recovery. Different with other gases, dissolution of  $\mathrm{CO}_2$  in water often causes the increase of the density. Because such density increase is generally not large, the accurate estimation of the pure water density is the necessity. In this work, we use a polynomial to describe temperature-dependent volume translation for pure water which is determined from the best fit of the difference of the saturated liquid molar volume between the experiments and calculations up to 600 K, i.e.,

Table 5. Same as Table 4 But for Vapor-Liquid-Liquid Equilibrium

			Composition (Mole Fraction)								
Temperature	Pressure			H <sub>2</sub> S Liqui	d		Aqueous			Vapor	
(K)	(bar)	Component	Exp	Cal(ca)	Cal(nca)	Exp	Cal(ca)	Cal(nca)	Exp	Cal(ca)	Cal(nca)
310.95	62.6	$\begin{array}{c} \mathrm{CH_4} \\ \mathrm{CO_2} \\ \mathrm{H_2S} \\ \mathrm{H_2O} \end{array}$	0.0653 0.1049 0.8197 0.0101	0.0616 0.0971 0.8292 0.0122	0.0642 0.0981 0.8369 8.85e-4	4.9e-4 3.5e-3 0.0284 0.9677	5.98e-4 2.61e-3 0.0310 0.9659	5.53e-4 2.54e-3 0.0276 0.9694	0.3213 0.1739 0.5028 2.14e-3	0.3596 0.1219 0.5169 1.63e-3	0.3527 0.1213 0.5248 1.26e-3
338.75	84.3	$\begin{array}{c} \mathrm{CH_4} \\ \mathrm{CO_2} \\ \mathrm{H_2S} \\ \mathrm{H_2O} \end{array}$	0.0580 0.0904 0.8287 0.0212	0.0641 0.0922 0.8264 0.0174	0.0674 0.0941 0.8358 2.72e-3	3.85e-4 2.72e-3 0.0321 0.9684	4.15e-4 2.47e-3 0.0326 0.9645	3.8e-4 2.17e-3 0.0346 0.9628	0.1872 0.1484 0.6557 8.66e-3	0.2057 0.1185 0.6704 5.44e-3	0.1919 0.1176 0.6870 3.52e-3

 $c_{\rm w} = a_0 + a_1 T_{\rm rw} + a_2 T_{\rm rw}^2 + a_3 T_{\rm rw}^3 + a_4 T_{\rm rw}^4 + a_5 T_{\rm rw}^5 + a_6 T_{\rm rw}^6$ where  $c_{\rm w}$  is the volume translation parameter in the unit of "L/mol" and  $T_{\rm rw}$  is the reduced temperature. The coefficients are  $a_0 = 0.1214789046$ ,  $a_1 = -1.1152038536$ ,  $a_2 = -1.1152038536$ 4.3159229705,  $a_3 = -8.9395416719$ ,  $a_4 = 10.3968272712$ ,  $a_5 = -6.4222352433$ , and  $a_6 = 1.6442114295$ . The AAD between the experiments and calculations is about 0.02% for the molar volume of pure water. The "true" molar volume of the mixture is calculated from  $v^{\text{True}} = v^{\text{EOS}} + (x_{\text{w}}c_{\text{w}} + c_{\text{w}}c_{\text{w}})$  $x_{\text{CO}}, c_{\text{CO}}$ ,) where  $v^{\text{EOS}}$  is the "apparent" molar volume obtained from the EOS. The volume translation parameter for CO2 is assumed to be a constant and determined from fitting the experiments of  $CO_2$ -saturated water densities ( $c_{CO_2}$ = -0.00314457 L/mol).<sup>31</sup> It should be noted that the value is different with that of pure CO<sub>2</sub> from the PR-EOS. CO<sub>2</sub> is a "special" substance compared with hydrocarbons because its saturated liquid densities cannot be matched by simply applying a constant volume translation to the results from the PR-EOS.

As displayed in Figure 11, a fairly good agreement is achieved between the experiments and calculations for the CO<sub>2</sub>-saturated water density in the examined temperature range by considering the volume translations for both water and CO<sub>2</sub>. The density of the CO<sub>2</sub>-saturated water strongly depends on the state of the coexisting CO2 phase. The sharp slope transitions at the low temperatures denote the CO<sub>2</sub> phase changes from vapor to liquid. For comparison, the densities of pure water are also calculated and plotted in the same figure. Under the examined temperatures and pressures, pure water is in the single-liquid phase. For all the cases, the density of the CO<sub>2</sub>-saturated water is always higher than that of pure water. The largest increase which is about 2% appears at the highest pressure of the lowest temperature and the difference becomes smaller as the pressure decreases or the temperature increases.

### **Conclusions**

The accuracy of CPA approach we proposed recently for the water-containing mixtures has been significantly improved by applying the "pseudo-association" concept. The unsaturated hydrocarbons, methane, ethane, CO2 and H<sub>2</sub>S are treated as pseudo-associating components, i.e., they only associate with water but do not associate with themselves. This cross association with water can be accurately described by using the same theoretical framework as the association of water molecules.

The cross association is likely due to polar-polar interactions between water and CO<sub>2</sub> or H<sub>2</sub>S or due to polar-induced

Table 6. Average Absolute Deviations of each Component for H<sub>2</sub>O/C<sub>1</sub>/CO<sub>2</sub>/H<sub>2</sub>S Mixture With and Without Cross Association

	AAD (%)				
Component	With cross Association (ca)	Without Cross Association (nca)			
CH <sub>4</sub>	7.59	6.70			
$CO_2$	8.21	8.28			
$H_2S$	4.11	5.91			
$H_2^-$ O	7.82	24.24			

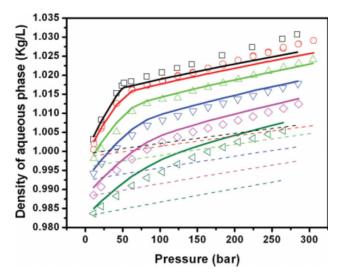


Figure 11. Density of CO<sub>2</sub>-saturated water (symbols: experiments from Ref. 31; solid lines: calculations) and of pure water (dash lines; calculations).

For each set, from top to bottom, the temperatures are 288, 293, 303, 313, 323 and 333 K. [Color figure can be viewed in the online issue, which is available at www. interscience.wiley.com.]

polar interactions between water and hydrocarbons, which has not been properly described by our previous CPA approach. For H<sub>2</sub>O/C<sub>1</sub> and H<sub>2</sub>O/C<sub>2</sub> mixtures, although C<sub>1</sub> and C<sub>2</sub> are saturated and nonpolar, the strong permanent polar moments of water molecules can cause the temporary separation of the centers of positive and negative charges of  $C_1$  and  $C_2$  molecules.

The modified approach enhances the accuracy in phase behavior calculations for H<sub>2</sub>O/C<sub>1</sub>, H<sub>2</sub>O/C<sub>2</sub>, H<sub>2</sub>O/CO<sub>2</sub>, H<sub>2</sub>O/ H<sub>2</sub>S, H<sub>2</sub>O/1-hexene, H<sub>2</sub>O/1-octene, H<sub>2</sub>O/1-decene, H<sub>2</sub>O/benzene, H<sub>2</sub>O/ethylbenzene, H<sub>2</sub>O/m-diethylbenzene, H<sub>2</sub>O/1methylnaphthalene, H<sub>2</sub>O/1-ethylnaphthalene, and H<sub>2</sub>O/C<sub>1</sub>/ CO<sub>2</sub>/H<sub>2</sub>S mixtures. We also reliably reproduce the density increase when water is saturated with CO2 by introducing the temperature-dependent and constant volume translations for water and for CO<sub>2</sub>, respectively.

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